

Amendments of the Rules

Part 15

Corrigenda 2 to Jan 2021 of Part 15



2022. 1. 06.

Hull Rule Development Team

Amendment

Note

Chapter 1 General principles

Section 2 - Rule Principles

5. Rule design method

5.3 Load-capacity based requirements

Table 1 : Load scenarios and corresponding rule requirements

Operation	Load type	Design load scenario	Acceptance criteria
Seagoing operations			
Transit	Static and dynamic loads in heavy weather	S+D	AC-SD
	Impact loads in heavy weather	Impact (I)	AC-I
	Internal sloshing loads	Sloshing (SL)	AC-SD
	Cyclic wave loads	Fatigue (F)	-
[omitted]	[omitted]	[omitted]	[omitted]

Sloshing loads for scantling(refer to **Ch 6, Sec 4, [2.7.2]** below) contains static pressure and impact pressure itself, acceptance criteria is modified to be correct as **AC-SD**.

The proposal of this corrigenda is to avoid unintentional and too conservative consequence effect for the current designs.

Chapter 6 Hull Local Scantling

Section 4 - Plating

2. Special requirements

2.7 Plating in cargo tank boundary

2.7.2 By sloshing pressure

The net thickness of plating, t in mm, subjected to sloshing pressures is not to be less than:

$$t = 0.0158 \alpha_p b \sqrt{\frac{P_{slh} + P_{ls}}{C_{a-slh} R_{eH}}}$$

[omitted]

β : Coefficient of AC-SD as defined in **Table 1**.

α : Coefficient of AC-SD as defined in **Table 1**.

C_{a-max} : Maximum permissible bending stress coefficient of AC-SD as defined in **Table 1**.

Refer to **Ch 1, Sec 2, [5.3] Table 1** above.

Amendment

Note

Section 5 - Stiffener**2. Special requirements****2.1 Section modulus of stiffener attached on cargo tank boundary****2.7.2 By sloshing pressure in cargo tanks**

The net section modulus Z in cm^3 , of stiffeners subject to sloshing pressure is not to be taken less than:

$$Z = \frac{|P_{slh} + P_{ls}| s \ell_{bdg}^2}{f_{bdg} C_{s-slh} R_{eH}}$$

[omitted]

β_s : Coefficient of AC-SD as defined in **Table 2**.

α_s : Coefficient of AC-SD as defined in **Table 2**.

C_{s-max} : Maximum permissible bending stress coefficient of AC-SD as defined in **Table 2**.

Chapter 3 Structural Design Principles**Section 7 - Structural Idealisation****1. Structural idealisation of stiffeners and primary support members****1.3 Effective breadth****1.3.1 Stiffeners**

The effective breadth, b_{eff} , in mm, of the attached plating to be considered in the actual net section modulus for the yielding check of stiffeners is to be obtained from the following formulae:

a) Where the plating extends on both sides of the stiffener:

$$\underline{b_{eff} = 100\ell} \quad \underline{b_{eff} = 200\ell}, \text{ or}$$

$$b_{eff} = 30\ell + 0.42s \quad b_{eff} = s$$

whichever is lesser.

b) Where the plating extends on one side of the stiffener (i.e. stiffeners bounding openings):

$$\underline{b_{eff} = 50\ell} \quad \underline{b_{eff} = 100\ell}, \text{ or}$$

$$b_{eff} = 0.15\ell + 0.21s \quad b_{eff} = 0.5s$$

Refer to Ch 1, Sec 2, [5.3] Table 1 above.

Current rule text regarding the effective breadth is found different from other KR Rules and CSR. It need to be in line with other Classification Societies' Rule including CSR.

Amendment	Note
whichever is lesser. [omitted]	