## Guidance for Ships for Navigation in Ice

## 2022. 02.



## Machinery Rule Development Team

## - Main Amendments -

(1) Effective date : 1 Jul. 2022 (Date of which contracts for construction are signed)

• The coefficients for fatigue design of propeller blade have been modified.

| Present   |                |                  |  |  | Note   |                  |  |
|---|----------------|------------------|--|--|--|------------------|--|
| CHAPTER 1 STRENGTHENING FOR<br>NAVIGATION IN ICE  |                |                  |  | CHAPTER 1 STRENGTHENING FOR<br>NAVIGATION IN ICE   |  |                  | <guidance fo<br="" for="" ships="">Navigation in Ice&gt;</guidance>  |
| Section 6 Propulsion Machinery (2018)   |                |                  |  | Section 6  |  |                  |  |
| 606. Design   |                |                  |  | 06. Design   | (Amendment)Modification<br>n of coefficients fo                  |                  |  |
| 1. 〈omitted〉  |                |                  |  | 1. (same as the pres   | fatigue design of pro  |                  |  |
| 2. Propeller blade  |                |                  |  | 2. Propeller blade   | peller blad<br><application date:="" td="" th<=""></application> |                  |  |
| <ul> <li>(1) ~ (2) ⟨omitted⟩</li> <li>(3) Fatigue design of propeller blade<br/>The fatigue design of the propeller blade is based on an estimated load distribution for the service life of the ship and the S-N curve for the blade material. An equivalent stress that produces the same fatigue damage as the expected load distribution shall be calculated and the acceptability criterion for fatigue should be fulfilled as given in this Section. The equivalent stress is normalized for 10<sup>8</sup> cycles.<br/>For materials having two slope S-N curve (See Fig 1.13) fatigue calculations according to this sub-paragraph are not required if the following criterion is fulfilled.</li> <li>σ<sub>exp</sub> ≥ B<sub>1</sub> • σ<sup>B<sub>2</sub></sup><sub>ref2</sub> • log(N<sub>ixe</sub>)<sup>B<sub>3</sub></sup></li> <li>where, B<sub>1</sub>, B<sub>2</sub> and B<sub>3</sub> coefficients for propellers are given in the table below.</li> </ul> |                |                  |  | S-N curve for the blade material. An equivalent stress that produces the same fatigue damage as the expected load distribution shall be calculated and the acceptability criterion for fatigue should be fulfilled as given in this Section. The equivalent stress is normalized for 10 <sup>8</sup> cycles.<br>For materials having two slope S-N curve (See Fig 1.13) fatigue calculations according to this sub-paragraph are not required in the following criterion is fulfilled.<br>$\sigma_{\rm exp} \geq B_1 \cdot \sigma_{\rm ref2}^{B_2} \cdot \log(N_{\rm icc})^{B_3}$ where, $B_1$ , $B_2$ and $B_3$ coefficients for propellers are given in the table below. |  |                  | I the 1 July 2022><br>pro-<br>ution<br>tigue<br>tress<br>tigue<br>ed if<br>- Reflects the effect of<br>the change of th<br>safety factor from 1. |
| Table 1.23         B1, B2   | Open propeller | Ducted propeller |  |  | 2 and B <sub>3</sub> coefficients                                | Ducted propeller | crease of the value C  |
| B_1   | 0.00246        | 0.00167          |  | B_1  | 0.00328  | 0.00223          | in Table 1.24.<br>- Reflects the correct   |
| B_2   | <u>0.947</u>   | 0.956            |  |  | <u>1.0076</u>  | <u>1.0071</u>    | tion of errors in the<br>calculation formula fo  |
| B_3   | 2.101          | 2.470            |  | B <sub>3</sub>   | 2.101  | 2.471            | calculating the co   |
| (hereafter, omitted)     efficients B <sub>1</sub> ,  |                |                  |  |  |  |                  |  |